



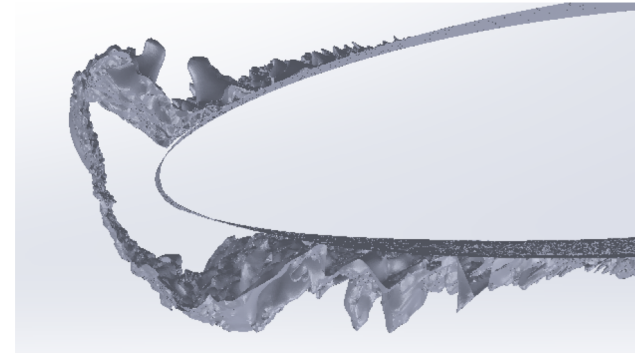
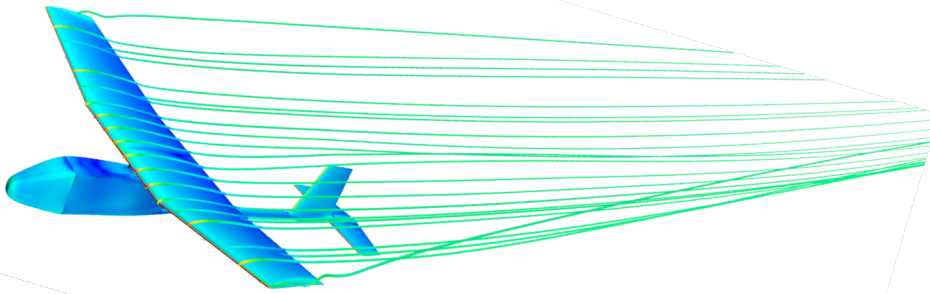
CAL POLY
SAN LUIS OBISPO

SJSU SAN JOSÉ STATE
UNIVERSITY

W UNIVERSITY of
WASHINGTON

Bay Area
Environmental | Research
Institute

Airborne science driven CFD of small UAS: Scalable airframe and ice accretion simulations



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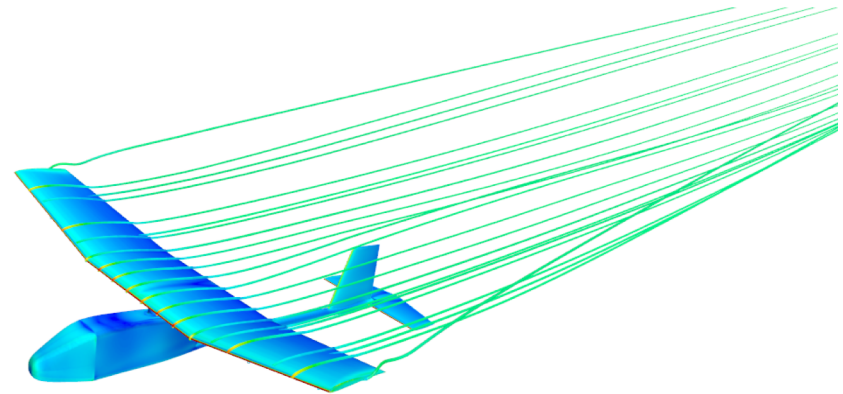
Mentors:
Robert Dahlgren
Tom Pulliam
Christopher Porter

AMS Seminar Series
NASA Ames Research Center
March 22nd 2018



Earth Science Drivers for CFD Analysis

- Quick validation of numerous but usually small changes to aircraft in order to accommodate a wide variety of unique science payloads
 - Addition of a pod-mounted payload; modified nose or fuselage to carry payload
 - Effect of adding NACA scoop or external pylon for gas sensing probe
 - Interaction of prop wash and ground effects on payload sampling
- Simulation of frequently-modified UAS
 - For new payload airworthiness certification
 - Pitot tube study, stability study, etc
 - Evaluate tradeoffs enabled by modularity
- Small UAS in all environments
 - In potential or actual icing-conditions
 - Icing, crosswinds, etc have outside effect





Project Goals and Outcomes

- Leverage access to unique tools in support of Airborne Science
 - Supercomputer resource allocation, straightforward request via HEC ebooks
 - Licenses to STAR-CCM+ and open source tools
- Document provisioning process and CFD setup for the next PI
- Performance of FrankenRaven and tradeoff study
- CFD on suspected pitot tube location for airspeed indication error
- Performance of dual-fuselage FrankenRaven with instrument pod
- Ice accretion CFD on three small UAS under different cloud conditions
- Validate icing CFD and wind tunnel at very low airspeeds
- Development and documentation of useful scripts and macros



Project 1: CFD of Modular Small UAS

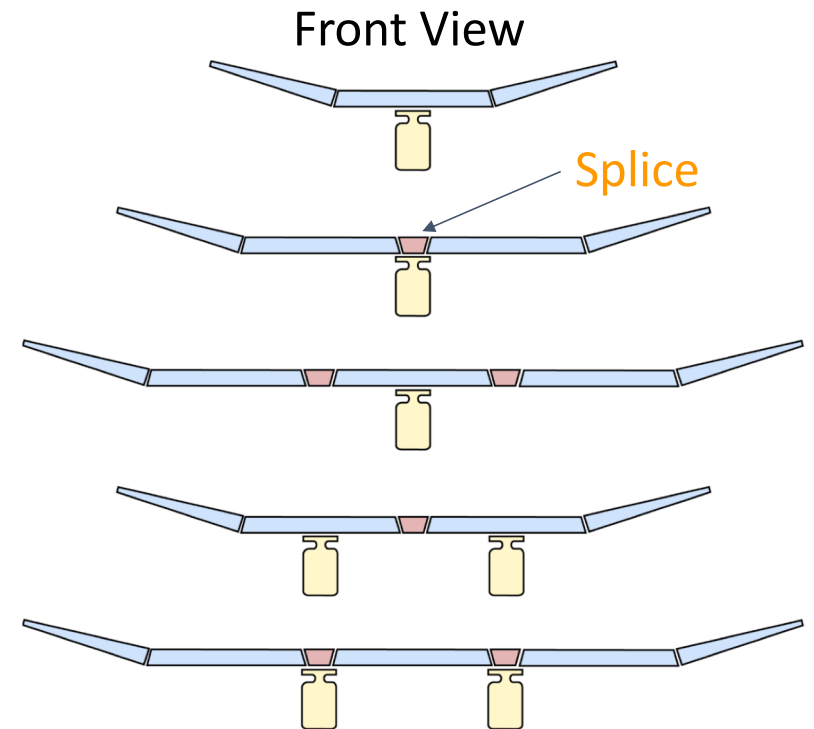
- Modularity for different airframe configurations
 - Multiple fuselage and wing modules
 - Variety of payloads and mission profiles
 - Even simple modularity creates a complex tradeoff space
- Advantages compared to non modular UAS
 - Can be reconfigured on-the-spot
 - Straightforward building and logistics
 - Simplified repairs in the field with spare modules
 - Possible to optimize the airframe around the payload
- Supports variety of ConOps (Concept of Operations)
- Small class I aircraft used to demonstrate/validate





Modular UAS Concept: Fixed Wing

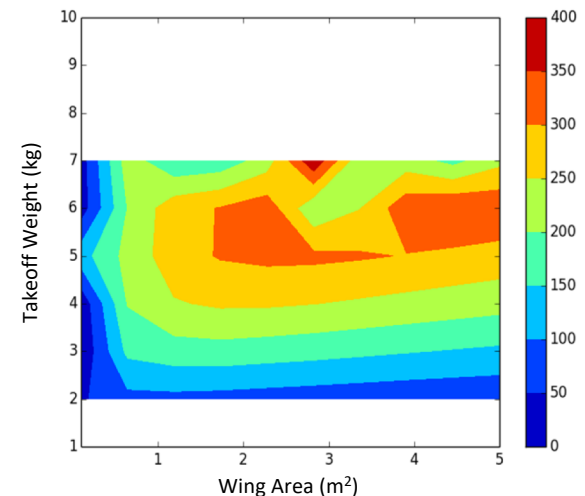
- Piecewise scalable fuselage, wing, battery, thrust, payload, and control surfaces
- Demonstrate the feasibility of modularity with UAS owned by ARC
- The UAS is segmented to facilitate fitting into a backpack
- Use as raw material for new aircraft
 - Connect wing segments with splice
 - Splice fabricated with 3D printing
 - Maximum splice count limited





Modular Framework Enables Tradeoff Space

- Modular aircraft is a new paradigm compared to fixed-configuration aircraft for science-driven applications; follows CubeSat model
- Modular aircraft opens up a new tradeoff space for mission design
- Studies in 2013 in 2014 showed that one of the most powerful variables in the aircraft performance tradeoff space is wingspan
- Number of wings (biplane, triplane)
- Battery count (also increases reliability)
- Payload weight (and ballast if any)
- Control surfaces (size, number, moment arm)
- Propulsors (number of thrust modules)





Considerations for Small UAS Flight Analysis

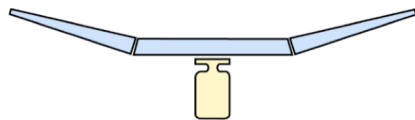
- Low speed operation: Mach 0.04
- FrankenRaven: Chord $D = 8.0''$ [203 mm]
- Low Reynolds number flight conditions
 - Between 130k to 400k
 - Large effective wing surface area at low velocity
 - Viscous drag is dominant, pressure drag is less of a factor
- Multiple configurations
 - Entails multiple envelopes of performance
 - Multiple payload capabilities to study

$$Re = \frac{\rho v D}{\mu}$$

$$\mu = 1.822 \times 10^{-5} \text{ Pas}$$

$$V = 10 \text{ m/s to } 30 \text{ m/s}$$

$$\rho = 1.225 \text{ kg/m}^3$$



OEM (Span = 1.3 m)

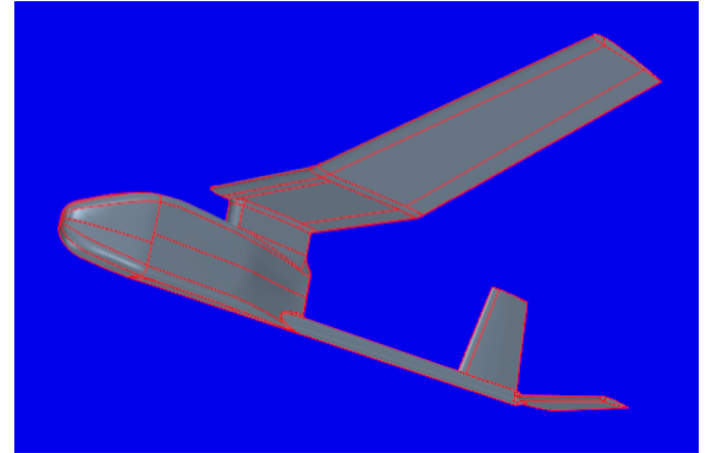


Largest Configuration (Span = 2 m)

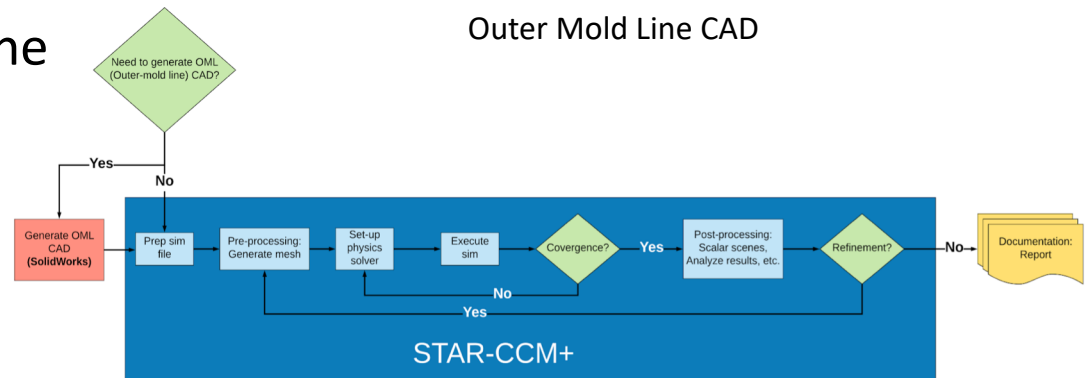


Workflow - FrankenRaven

- Convert assembly CAD to OML
- STAR-CCM+
 - Utilized built-in solver and mesh tools
- Steady State Reynolds Averaged Navier-Stokes
- Spalart-Allmaras turbulence modeling
 - Low airspeed
 - Expected minimal separation
- Hemispherical domain
- Mirror symmetry about the XZ plane
 - Set up for utilizing same mesh across wide range of velocities and AoA
 - 30 m radius, ~200 chord lengths away



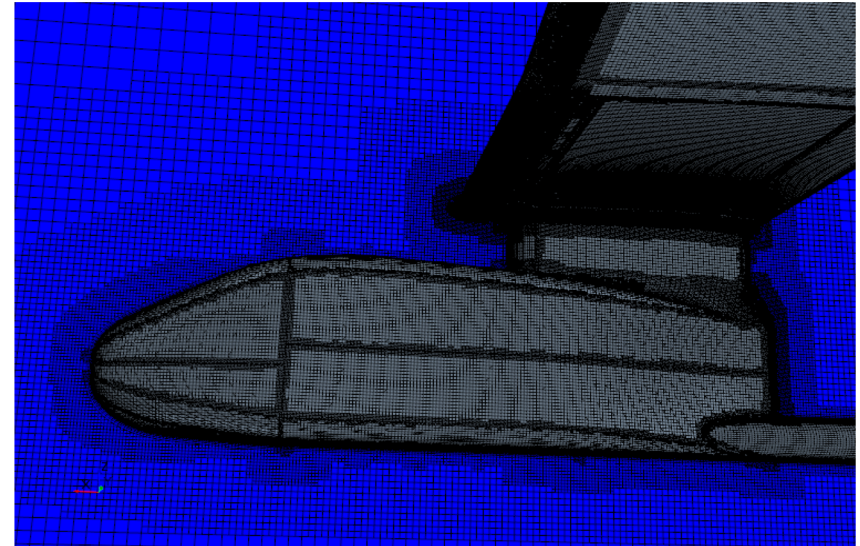
Outer Mold Line CAD





Meshing Approach 1: Trimmer

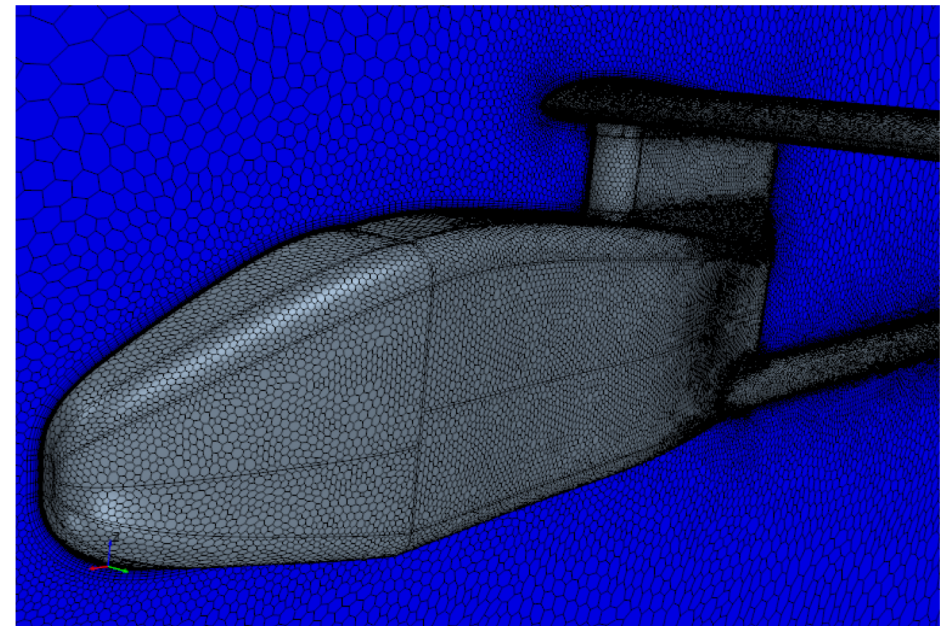
- Trimmer mesh (STAR-CCM+)
 - Unstructured
 - Majority of cells are exact cubes
 - ~12 million cells to simulate FrankenRaven
- Computationally efficient to both mesh and solve
- Difficult to capture blended areas e.g. the wing-to-fuselage pylon on the small UAS
 - Numerous small radius-of-curvature features
 - Accurate modeling demands high local cell count
- Was labor-intensive to get a high fidelity mesh





Meshing Approach 2: Polyhedral

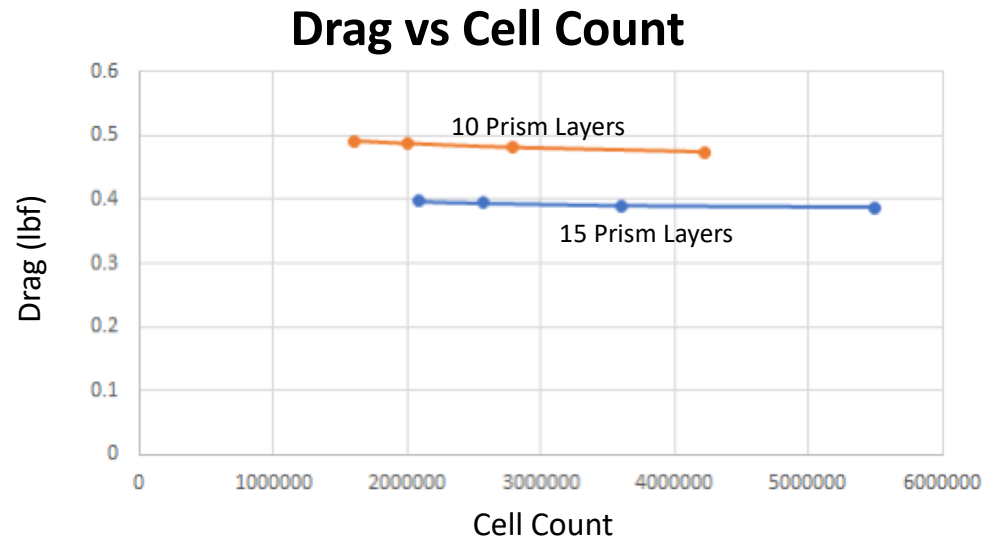
- Polyhedral mesh (STAR-CCM+)
 - Unstructured
 - Cells are 3D polyhedrons with variable face count and arbitrary angles
 - ~3 million cells to simulate FrankenRaven
- Computationally efficient solving
 - Similar residual quality
 - Solved in half the time compared to trimmer
 - Smaller file size
- Lesson learned: polyhedral more efficient for our application





Mesh Convergence

- Important for sweeps
 - Minimize cell count/computation
 - Large effects for large sim sweeps
- Parameters of Interest
 - Base size
 - Local cell size
 - Prism layer attributes
- Change in key parameters
 - Lift and drag
 - Residuals
 - Solver time
- Also tested at high and low AoA and airspeed for worst case scenario





States to Simulate

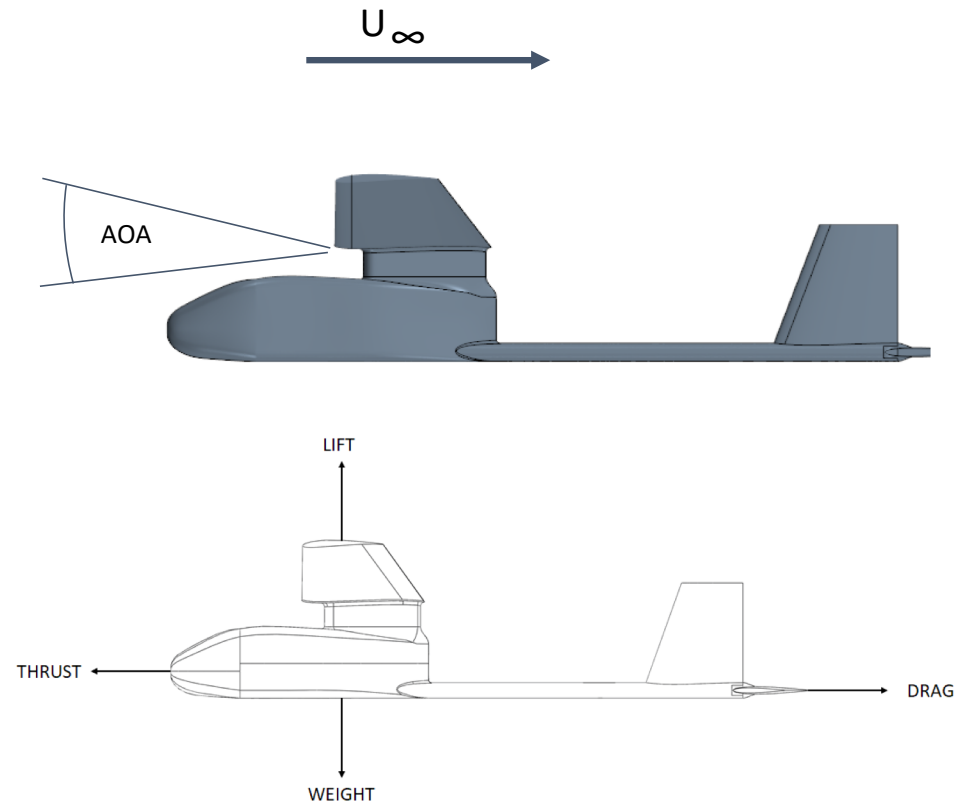
- Solve for constant given climb rate
- Optimize for maximum time on station (minimum power consumption, maximum efficiency, usually just above stall speed)
- Solve for a constant given cruise velocity (constant altitude) equilibrium
 - Thrust must equal drag
 - Lift greater than or equal to aircraft weight
 - Flow has not stalled yet
- Optimize for maximum distance (~ maximum velocity)
- Glide conditions (for FRRB)
- Maneuvers and landing (g-loading for FRRB)

THIS PRESENTATION



Simulation Sweeps

- 5 configurations
 - Minimize cell count/computation
 - Save time for large sim sweeps
- AoA from -10 to 20
 - Similar to XFOIL and UIUC database
 - Capture zero lift condition
 - 2 degree increments
- Post-processing
 - MATLAB and Java macros for exporting
 - Linear trends for lift and drag
 - Center of pressure for stability





Thrust and Range Calculations

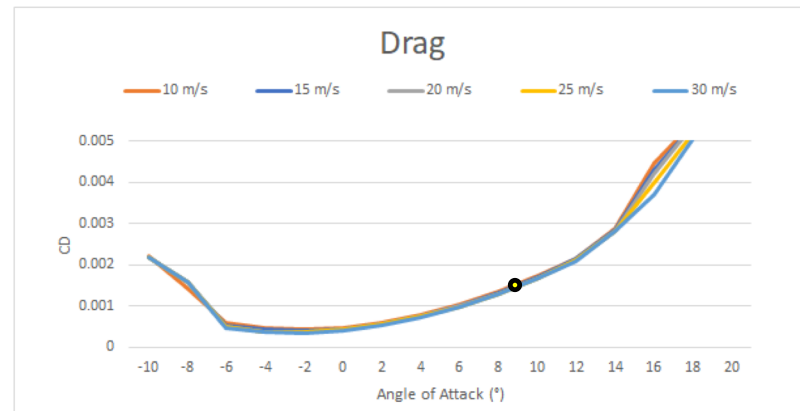
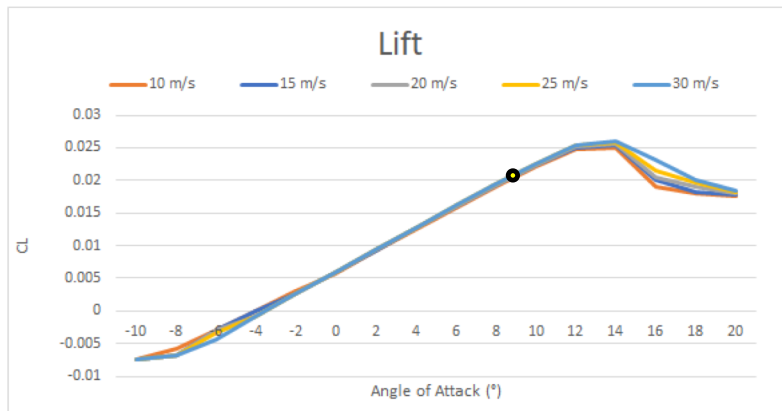
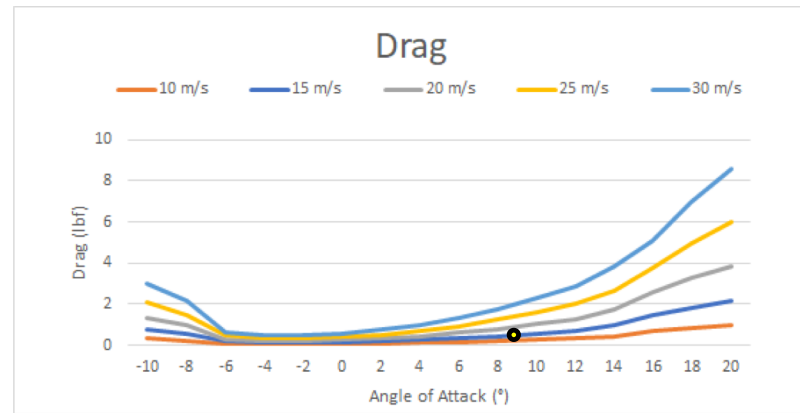
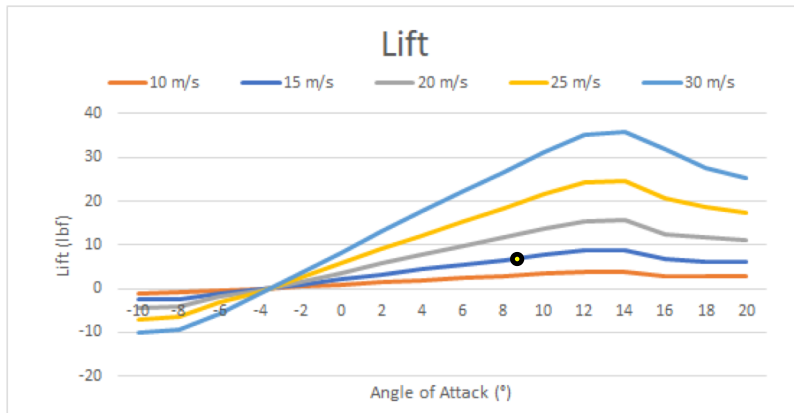
- Dynamic thrust used as approximation for this study
 - Used for rough thrust calcs in radio control aircraft
 - Function of pitch, RPM, and airspeed
- Equivalent drag used for power required
 - 85% efficiency
- Thrust as a function of propeller specifications, RPM, and airspeed
- Calculations done assuming no margin
 - Margin needs to be included for safety

$$\text{Power} = \text{Drag} * \text{Velocity}$$

$$\text{Flight Time} = \frac{\text{Voltage} * \text{Capacity}}{\text{Power}}$$



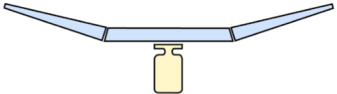
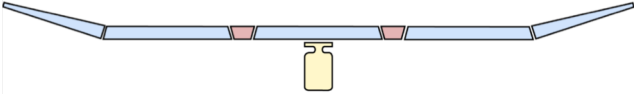
Points of Equilibrium (OEM)





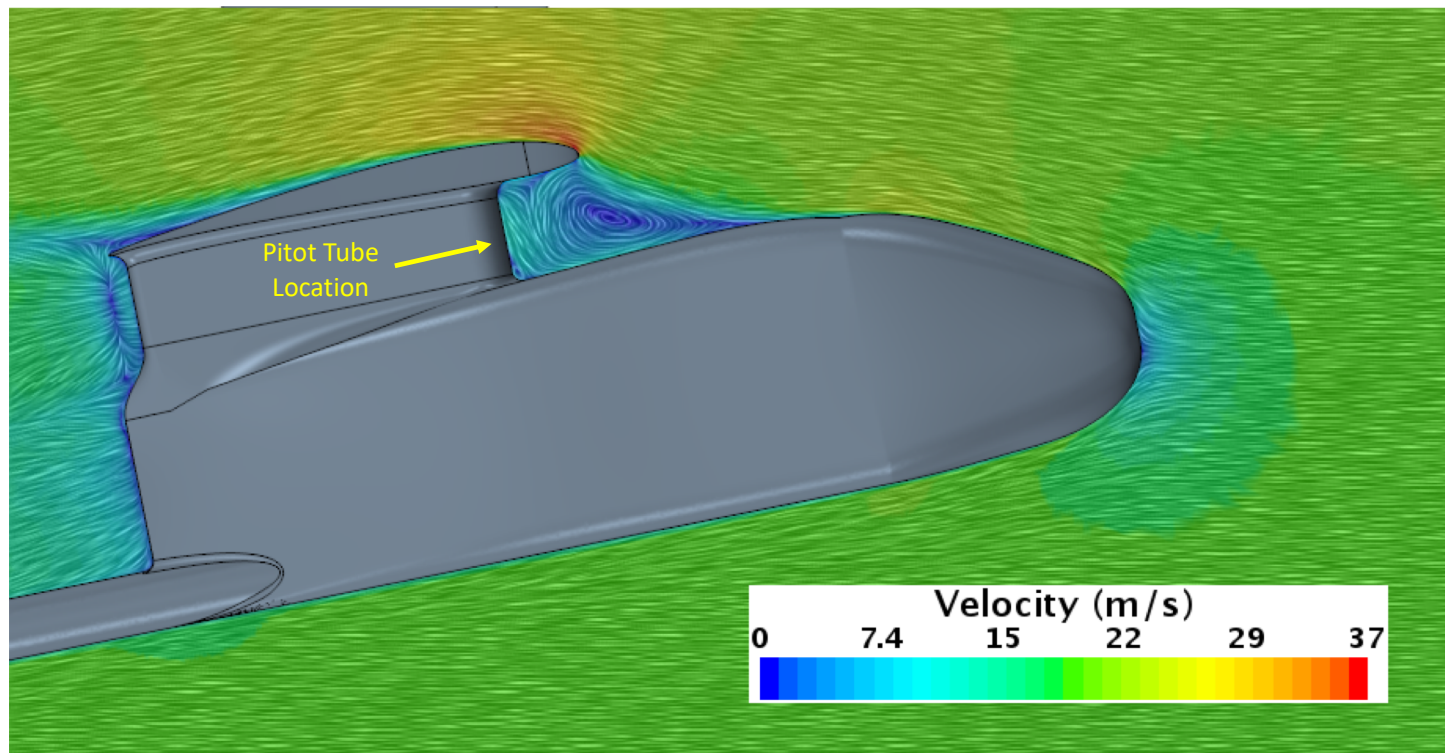
Payload Capabilities from Equilibrium Points

(*For dual-fuselage configurations, indicated margins are for a 2.67 lb payload)

<u>Configuration</u>	<u>AOA</u>	<u>Velocity</u> (m/s)	<u>Lift</u> (lbf)	<u>Payload*</u> (lb)	<u>Range</u> (km)	<u>Time</u> (min)
	8.3	15	6.7	2.5	27.6	31
	10.5	15	12.1	7.3	27.6	31
	3.4	15	9.1	3.7	27.6	31
	8.8	15	11.4	6.1 (56% margin)	27.6	31
	8.0	15	14.8	7.9 (66% margin)	27.6	31



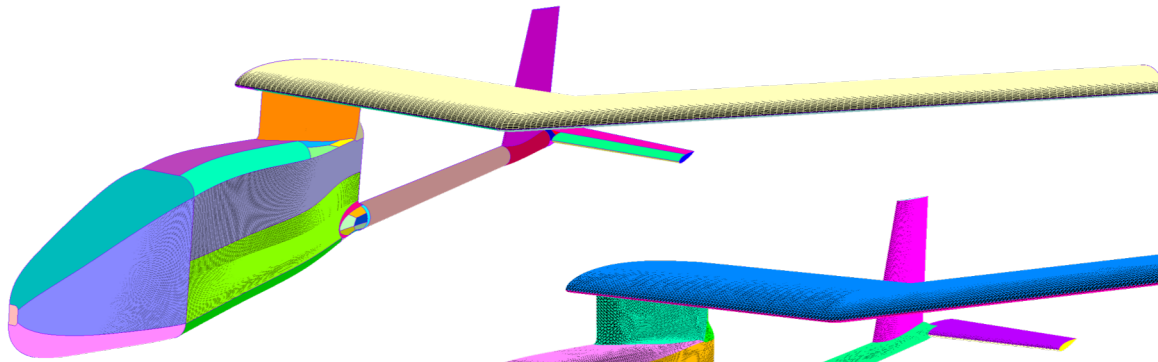
Pitot Tube Turbulence



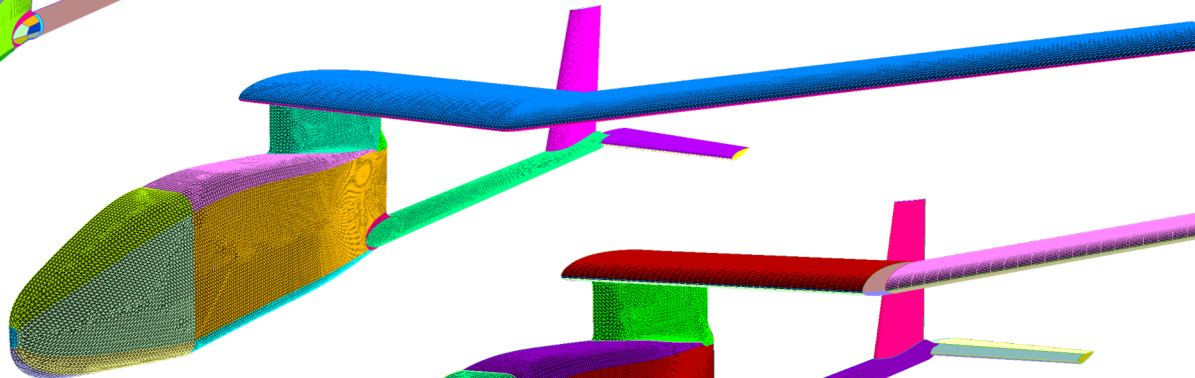
May explain autopilot issues when climbing at high AoA



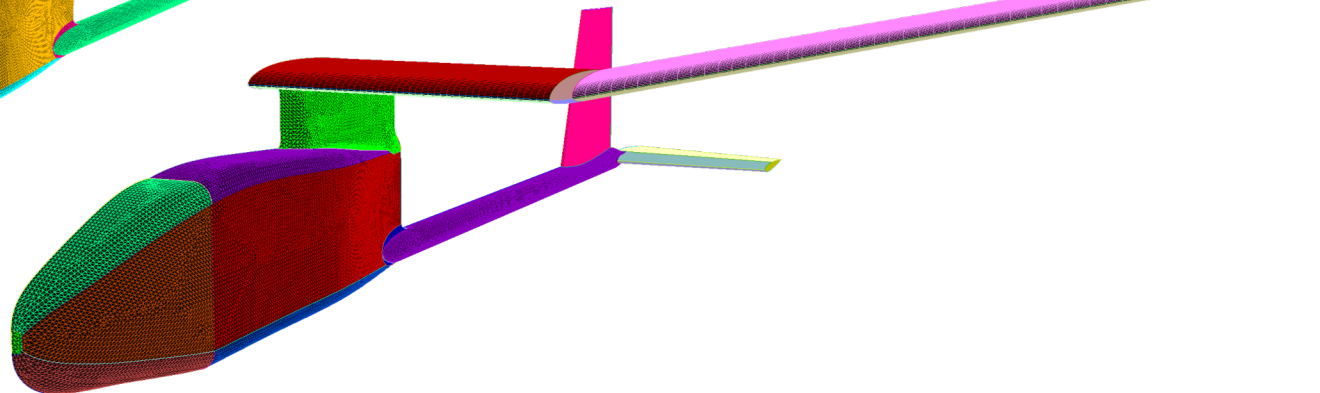
Meshing Alternative



Structured



Unstructured

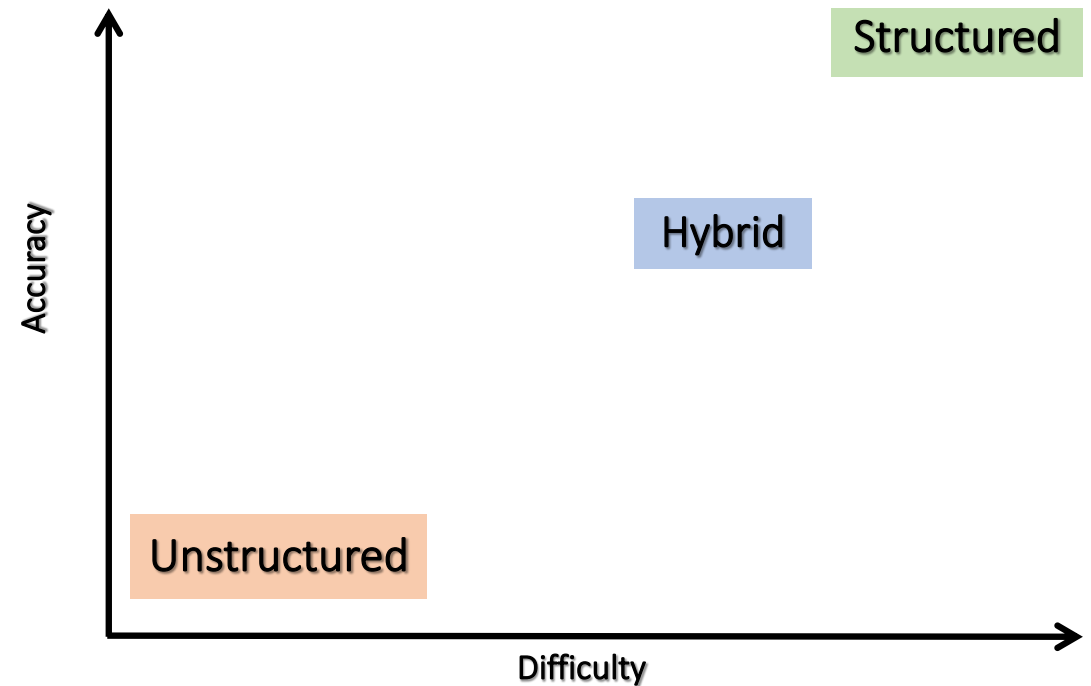


Hybrid



Meshing Alternative

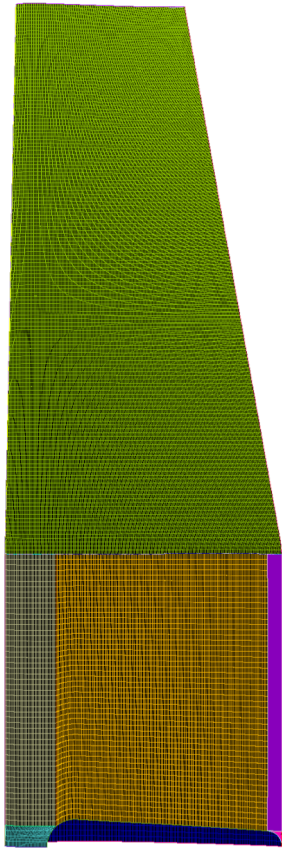
Structured	Unstructured	Hybrid
Low cell count	High cell count	Low cell count
Pre-processing is time consuming	Pre-processing is inexpensive	Pre-processing varies depending on geometry
Hexes comprise of quads	Tets comprised of tris	Compromised of tets, hexes, prisms, and pyramids
~ 1.78 million cells	~ 6.2 million cells	~ 2.8 million cells



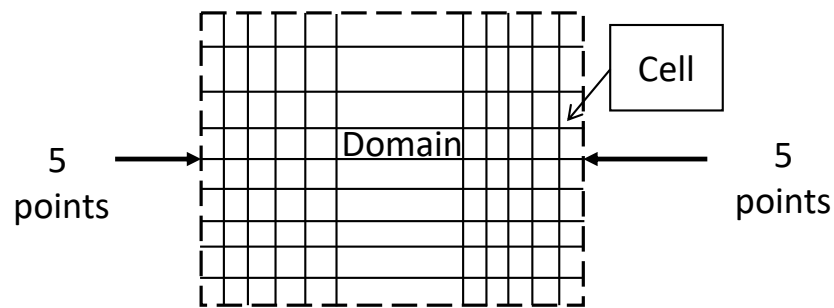
Modified from: Tim Baker, "Mesh generation: Art or Science?", Progress in Aerospace Sciences 2005



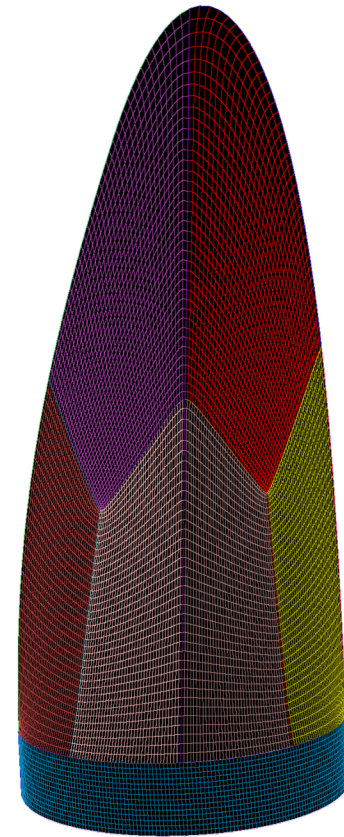
Structured Mesh



Wing section



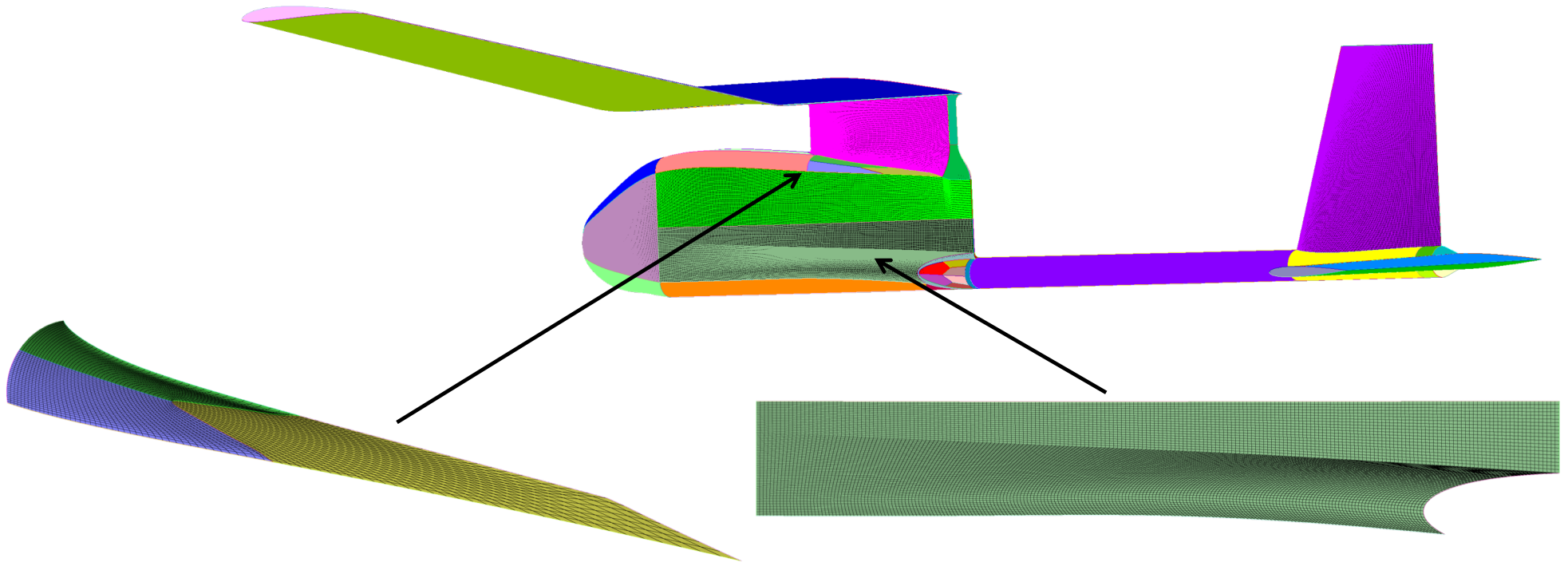
- Opposite edges have to match on the domain
- Each domain is colored differently
- Main goal is to drive cell count down



Tailboom – partial view₂₀



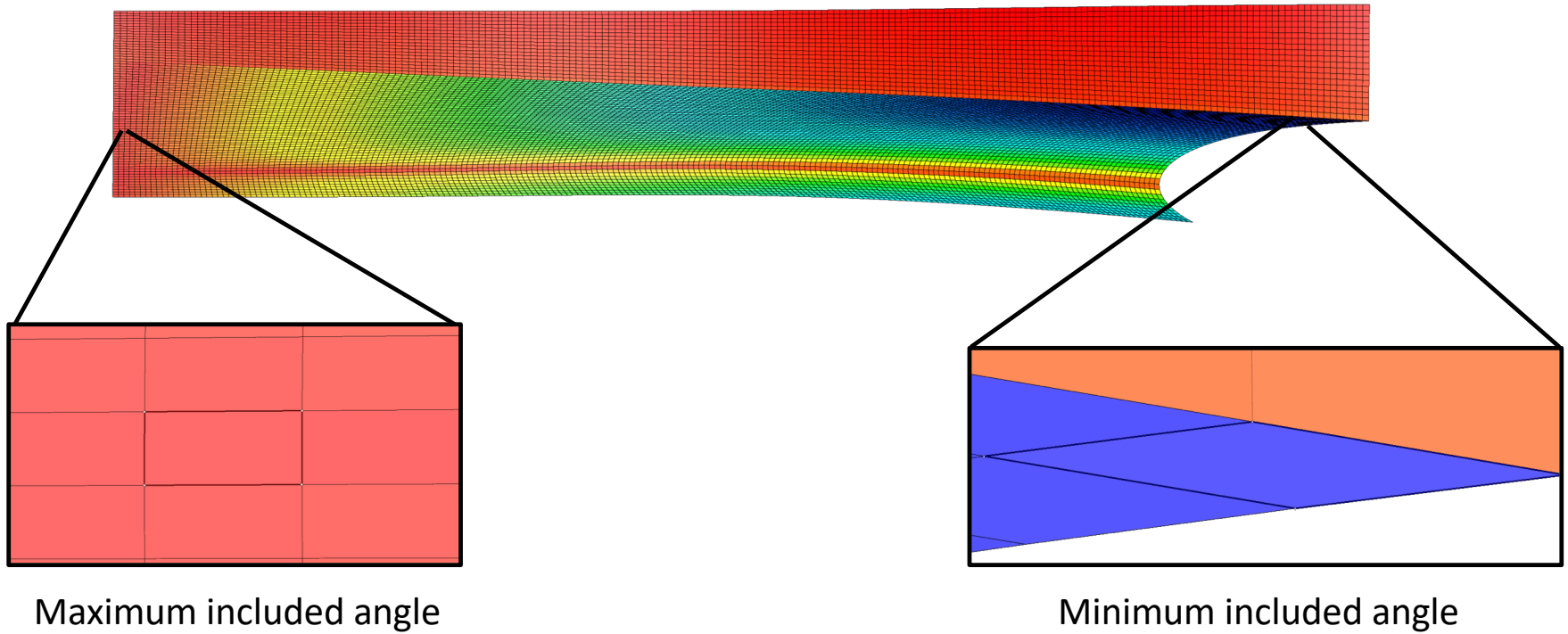
Structured Mesh



High skewness

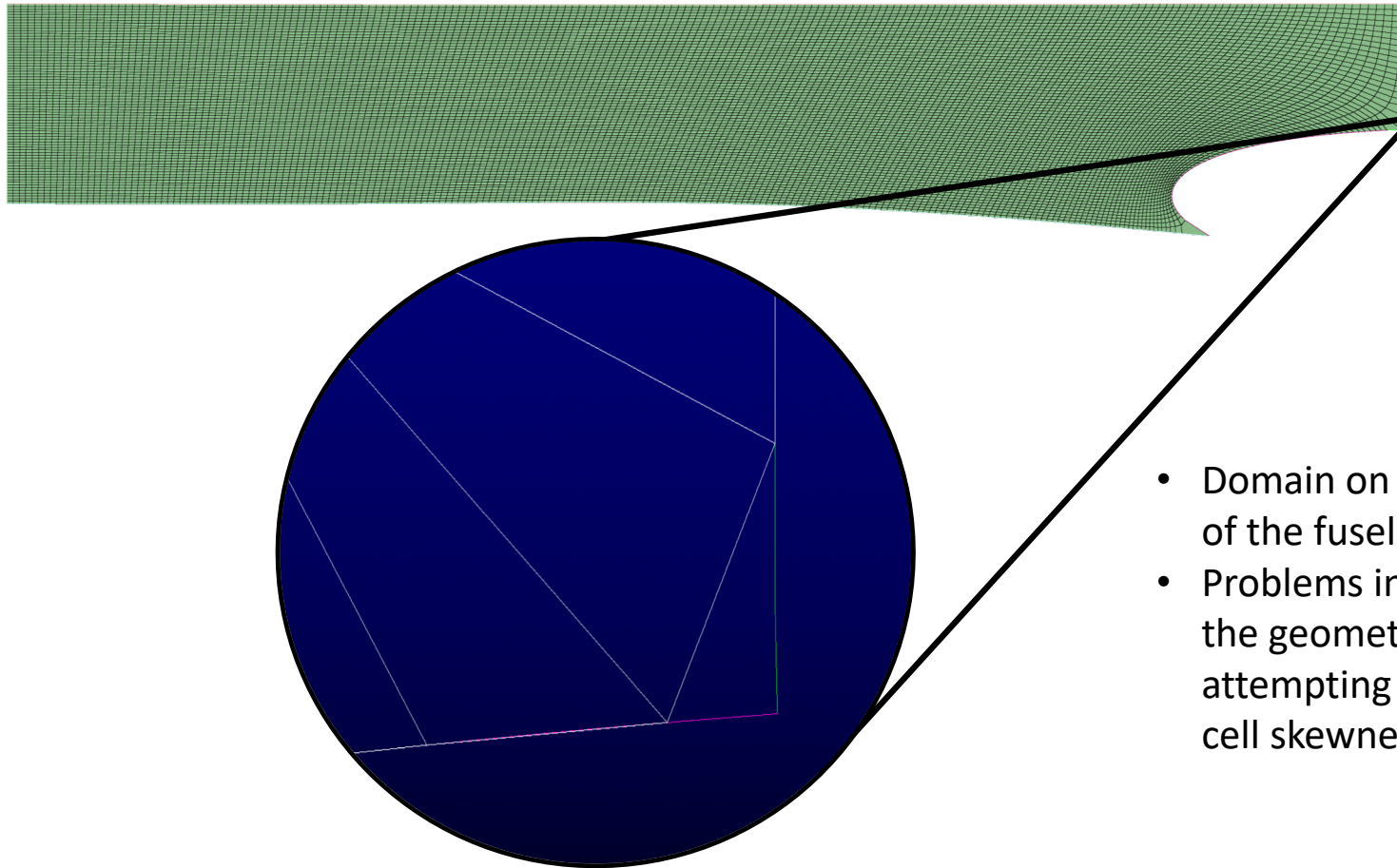


Structured Mesh





Structured Mesh

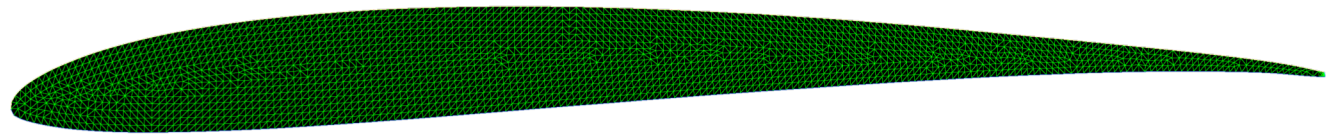


- Domain on the section of the fuselage
- Problems in recovering the geometry while attempting to resolve cell skewness

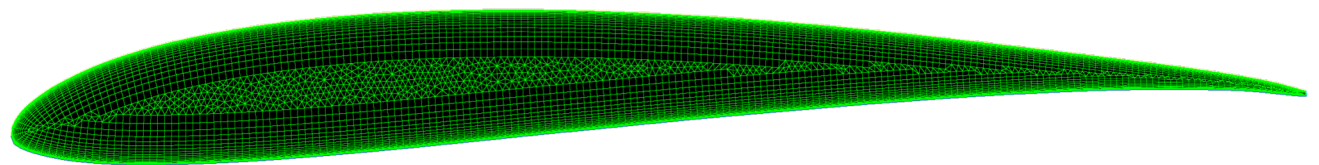


Hybrid Mesh

- T-Rex is an anisotropic tetrahedral extrusion method developed by Pointwise
- It is a highly automated and robust technique for generating unstructured boundary layer meshes for complex geometries
- Helps with resolving high curvature surfaces
- Reduces time in generating the volume mesh



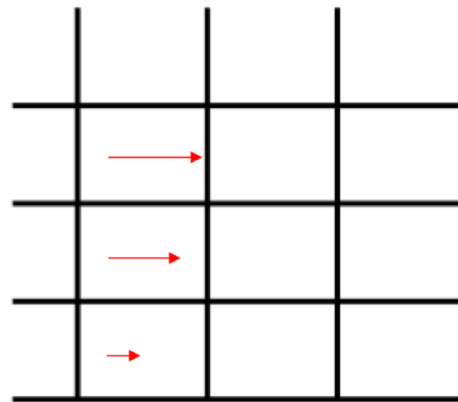
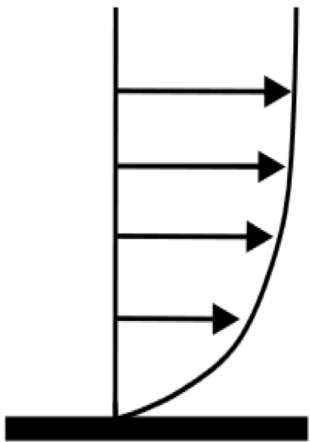
Without T-Rex



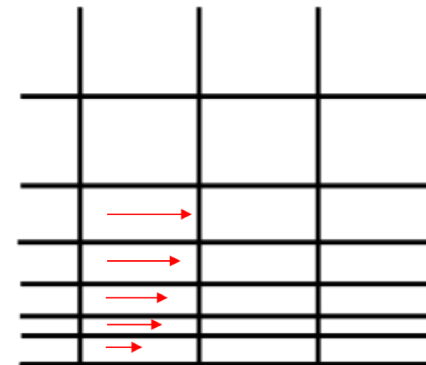
With T-Rex



Hybrid Mesh



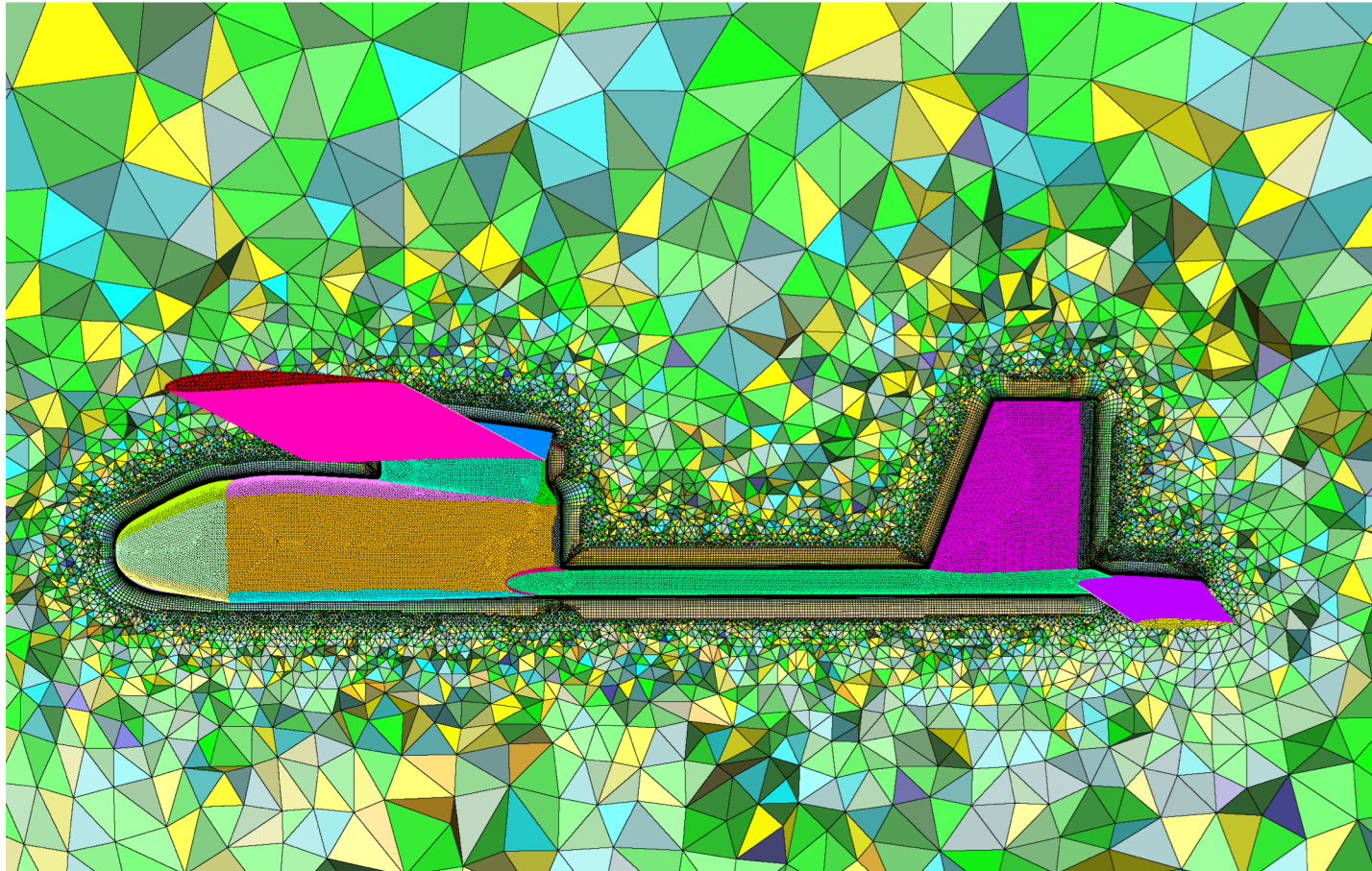
Inadequate resolution near
the wall



Better quality in resolving the
flow features



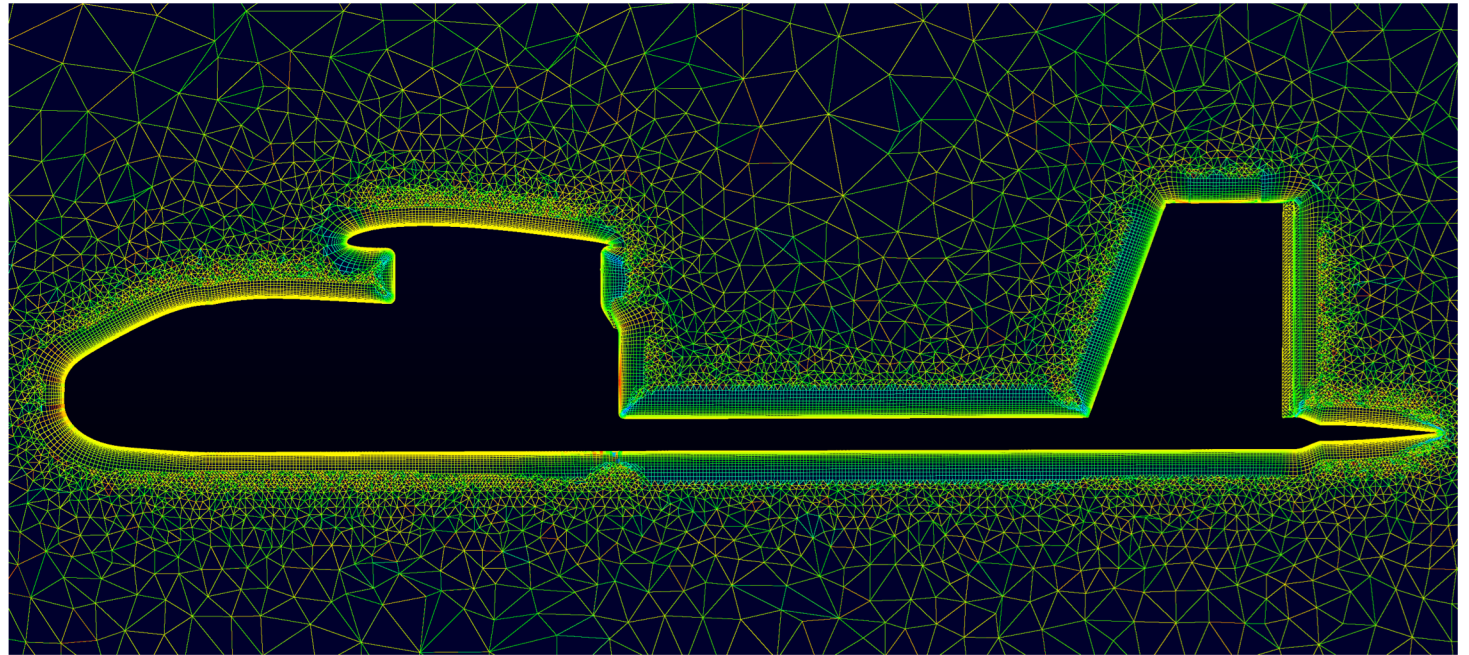
Hybrid Mesh





Hybrid Mesh

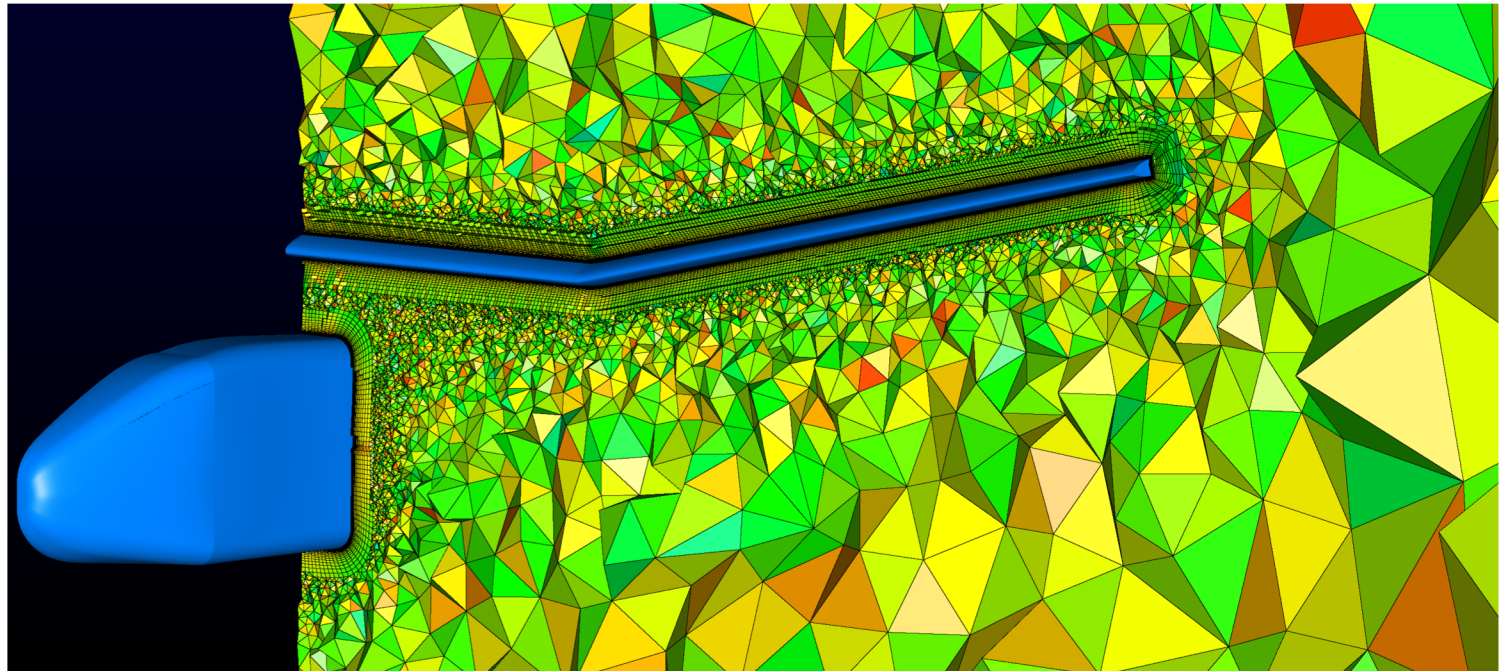
- Better control of cell size transition with the boundary decay parameter
- Increase boundary decay to prevent erratic jumps in cell size
- Quality cell transitions translates to a more accurate modeling of the flow








Hybrid Mesh

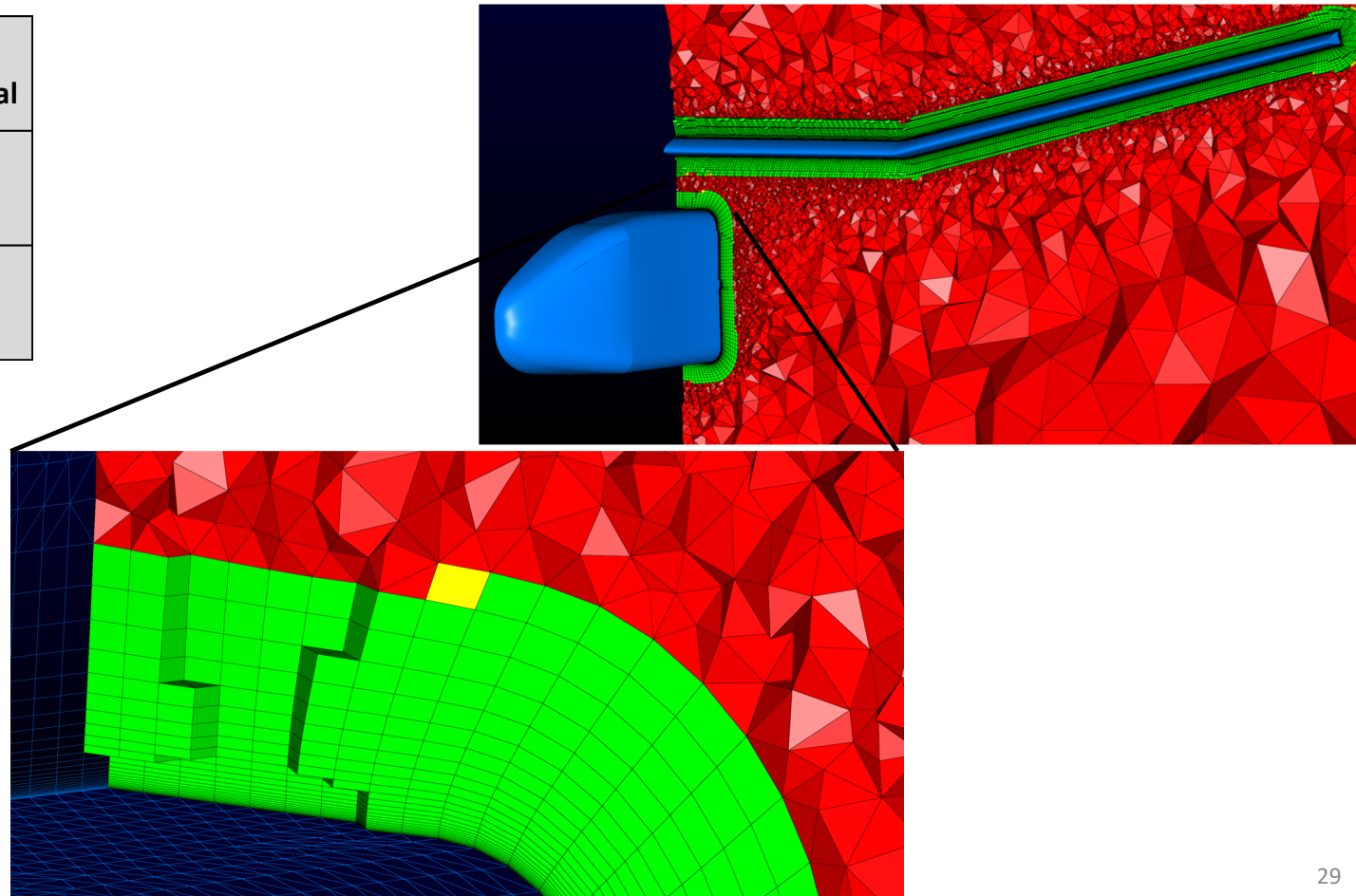
- Volume mesh in the unstructured block
- Made up of tetrahedrals, pyramids, and prisms
- Generated using T-Rex





Hybrid Mesh

	Tetrahedral
	Pyramid
	Prism





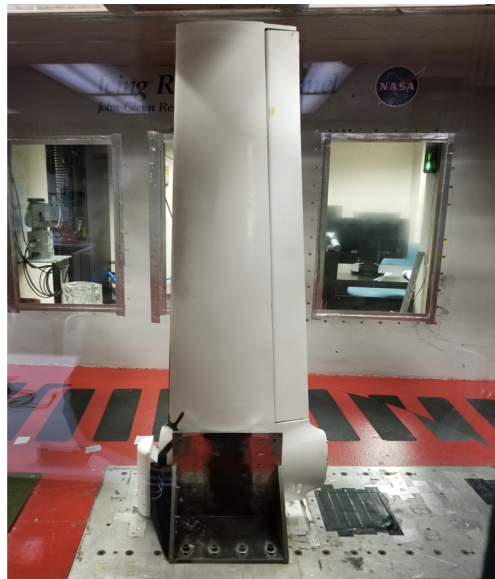
Future Considerations

- More equilibrium points
 - Every configuration has a range of steady flight conditions
 - Each range holds key information to flight capabilities
- Further stability analysis
 - How wingspan affects ease of control
 - Simulate lateral conditions
- Simulate flutter and aero-elasticity
- Smaller sweep increments
- Validation
 - Test steady level conditions
 - Static and dynamic thrust tests
- Concept extensible to larger aircraft



Part 3: Aircraft Icing of Low Speed Small UAS

- Test three small UAS in the Icing Research Tunnel to characterize ice accretion at different flight and icing conditions
- Validate LEWICE3D ice accretion research code for low speed small UAS
- Develop and investigate methodologies of quantitative comparison between experimental and simulation ice shape data





Why UAS?

- Lot more interest in Arctic Regions (Climate Change, Trade Routes, Geopolitics)
- More and more common now as their operating costs are much cheaper
- Able to maneuver in more extreme environments
- Are expendable, and do not risk safety of pilots





Motivation: SIERRA Incident

- 2013 - NASA SIERRA Aircraft lost engine power due to potential icing in Alaska





sUAS Icing vs Large Aircraft Icing

- Icing Research Tunnel Testing at NASA Glenn since 1944
- Our test was the first time UAS was in the IRT
- Weight of ice added in proportion to weight of UAS is much bigger
- More drastic change in performance characteristics
- Large aircraft fly fast enough where the aerodynamic forces form the shape of the ice
- Small UAS fly at a speed where gravity may have to be taken into account in ice formation models (not currently in LEWICE3D code)





Test Articles

DataHawk

- Designed/manufactured by University of Colorado
- Electric Motor Flying Wing, Pusher Propeller
- Used by DOE at Oliktok Point, Alaska
- Collect measurements of lower atmospheric properties
- Looking to develop de-icing systems



ArcticShark

- Designed/manufactured by Navmar Applied Sciences Corporation
- Internal combustion engine, pusher propeller
- Weather-tolerant version of TigerShark
- Airborne atmospheric research drone to measure radiative, aerosol, and cloud properties
- Produces 4000 W, 2500 W dedicated to payload



Outlaw SeaHunter

- Designed/manufactured by Griffon Aerospace
- Platform for ISR missions, system tests, R&D, and payload development
- Flew in Canada successfully operating at 15,000 feet at -40 C in Feb 2018

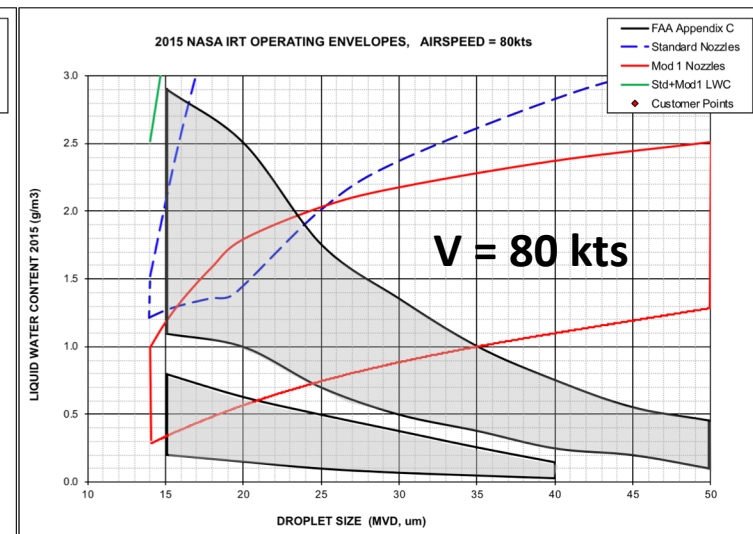
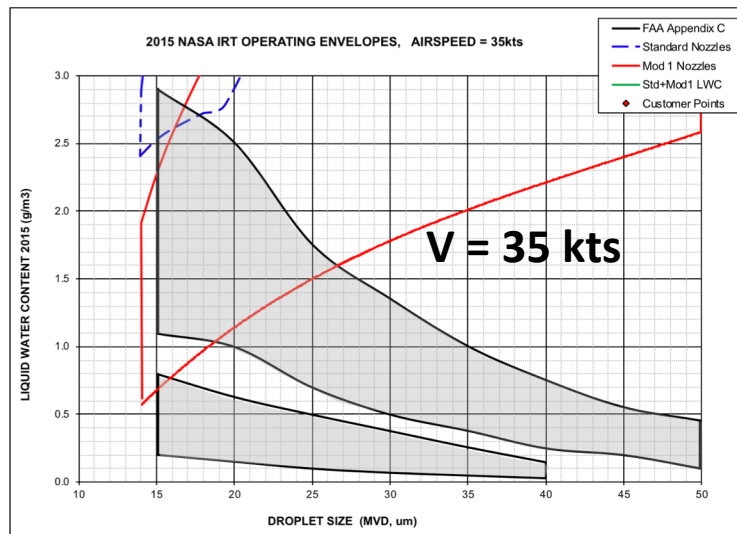




Flight and Icing Cloud Conditions

- Cruise velocities and typical climbing AoA
- Temperature: -10 C (Glaze Ice) and -20 C (Rime Ice)
- Mean Volume Diameter (MVD): 15, 25, 50 μm
- Liquid Water Content (LWC): 0.5, 1.5, 2.0 g/m^3
- Exposure time: 10 minutes

*Cloud conditions were chosen to match corner cases from FAA Appendix C Icing Certification Criteria within IRT operating envelopes



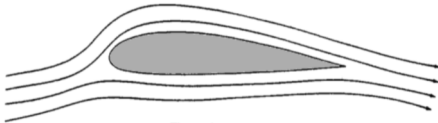
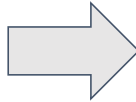


LEWICE3D Overview

- Research Code by NASA Glenn Research Center
- Simulate ice accretion on 3D aircraft surfaces (in Quasi-3D)

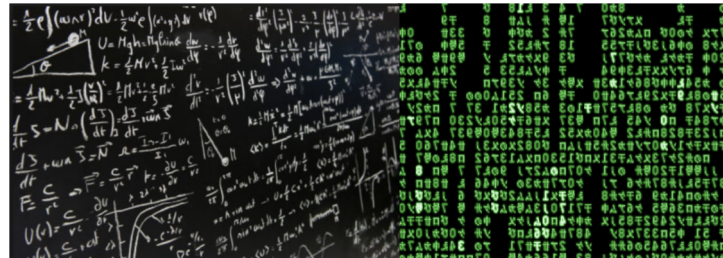
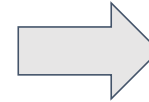
Inputs

- Aerodynamic Flow Field
- Icing cloud conditions



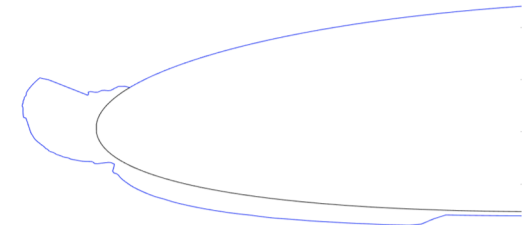
Computational Module

- Calculate approaching water droplet trajectories
- Calculate mass and energy transfer on surface
- Modeling freezing process in finite control volumes



Outputs

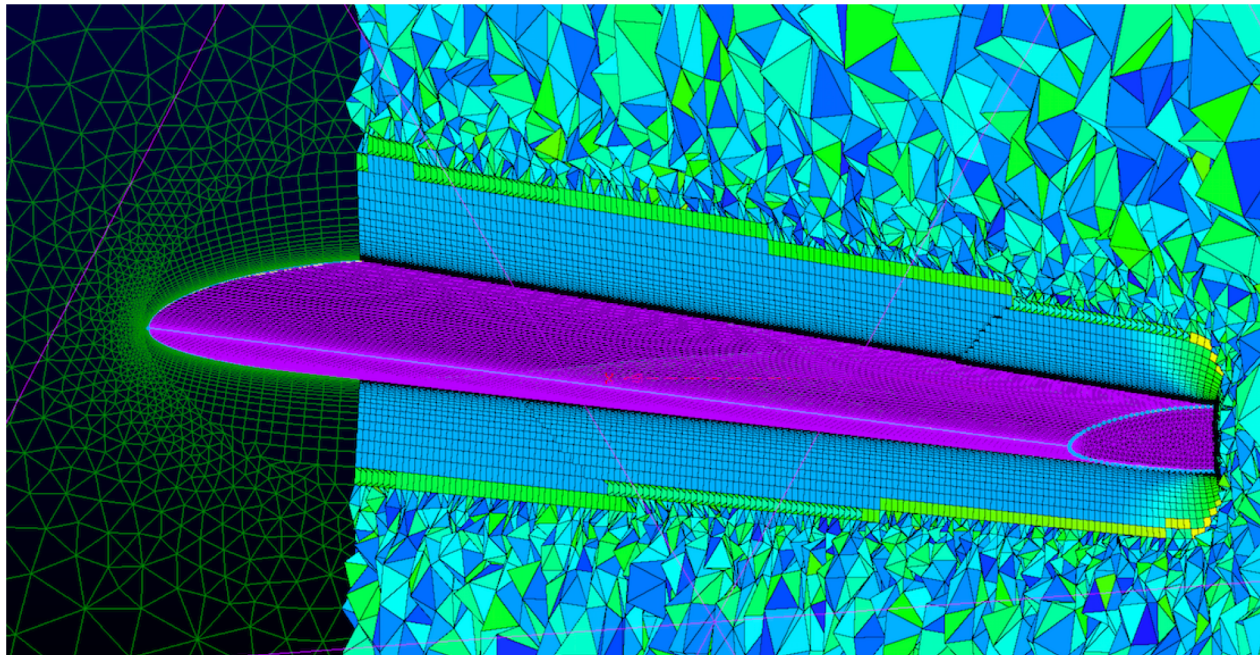
- Ice shapes at 2-D section planes of interest





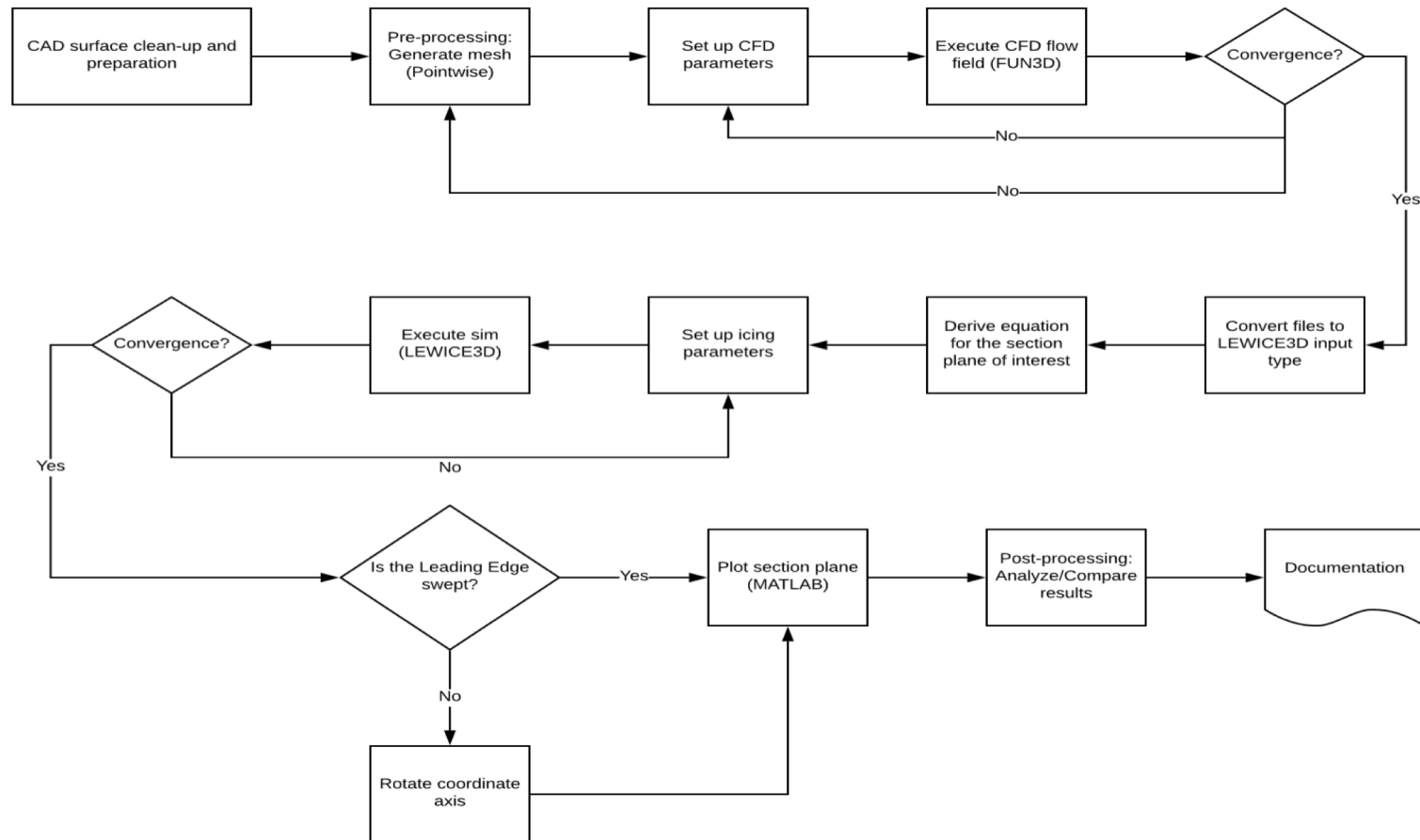
Meshing/CFD for Ice Accretion Simulations

- Same best practices as Low-Reynolds Number Incompressible Flow CFD Meshing
- Unstructured tetrahedrals in fluid domain with structured quads to capture surface resolution
- Boundary Layer Resolution
- Used NASA FUN3D Flow Solver





Methodology – Simulation of Ice Accretion

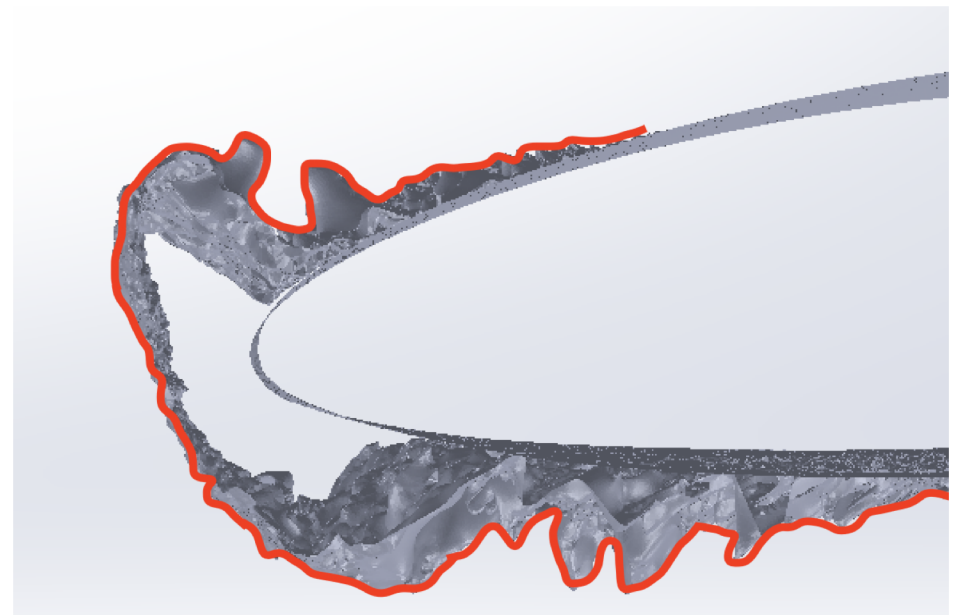




Methods of Quantitative Comparison

- Used high resolution robotic arm 3D scanner to capture experimental ice shape
- Maximum Combined Cross Sectional Area*

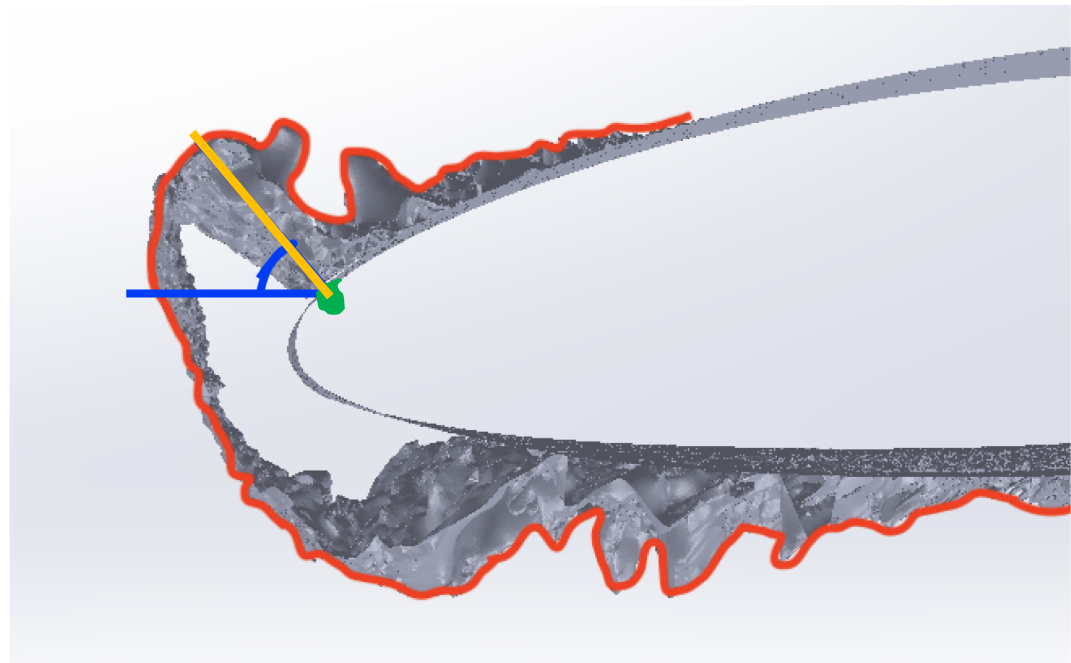
*For swept wings, perpendicular to LE





Methods of Quantitative Comparison

- Find largest horn perpendicular to aircraft surface
- Horn Location
- Horn Length
- Horn Angle

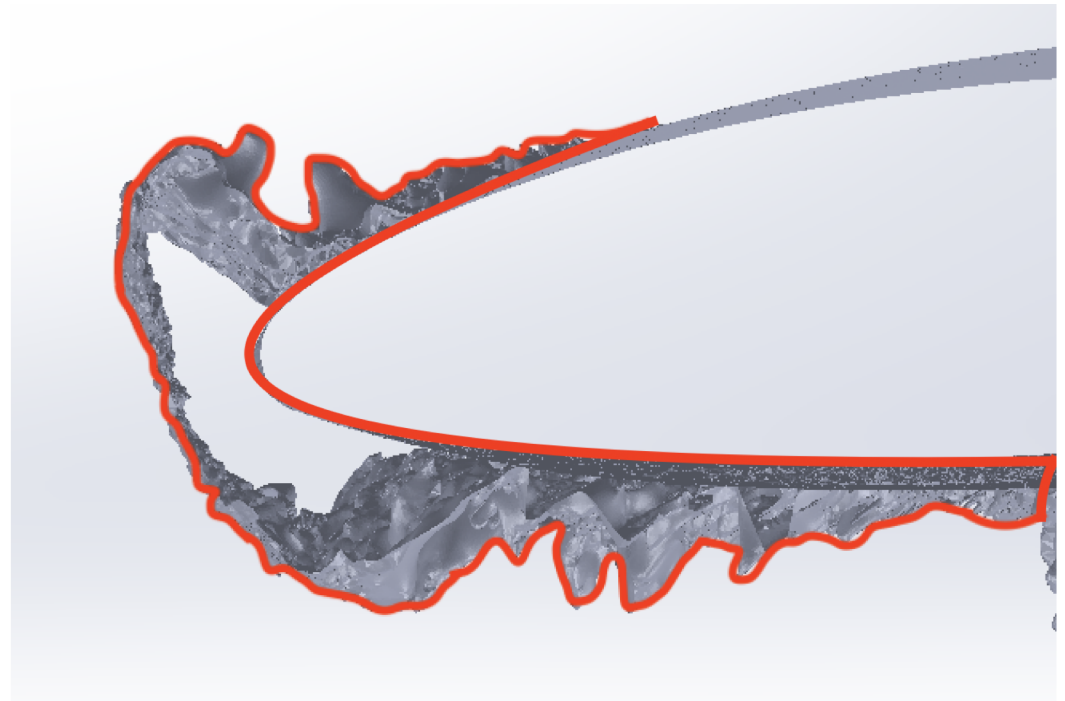




Methods of Quantitative Comparison

- Area/Volume of Ice
- Estimated Mass*

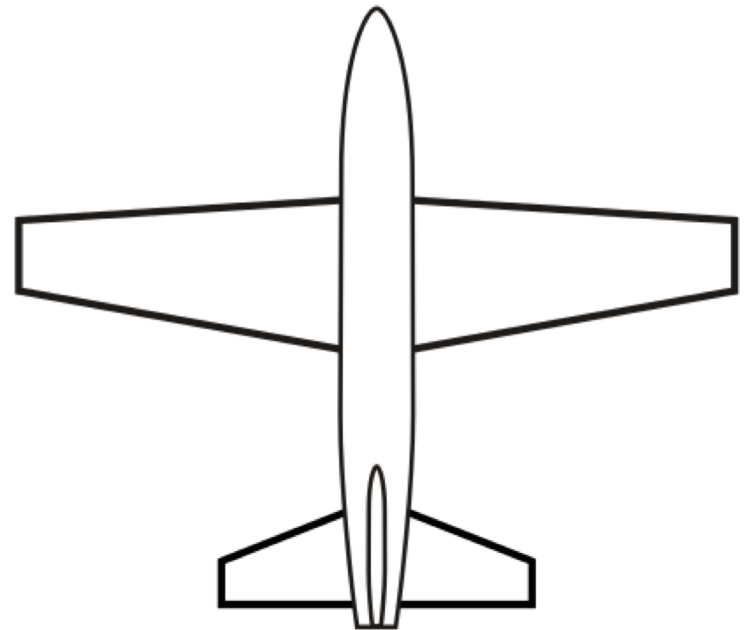
*Previous studies have used a density of 450 kg/m^3 to account for voids throughout the span





Tapered Wings

- Max Combined Cross Section fails
- Chord/thickness not consistent
- Limited to comparing single cut sections
- SeaHunter and DataHawk faces this problem



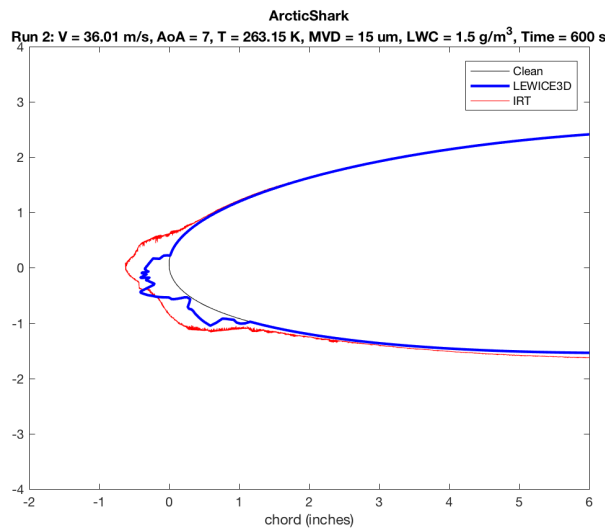


ArcticShark: Glaze Ice (-10 C), AoA = 7, V = 70 kts

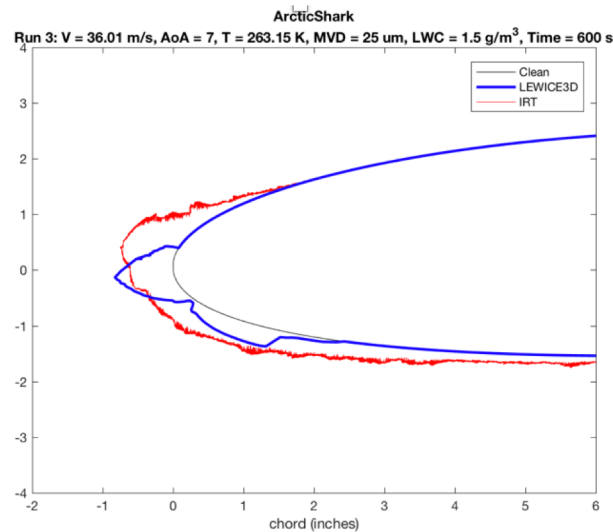
Glaze Ice = Water droplets do not freeze immediately upon impact

Experimental Data

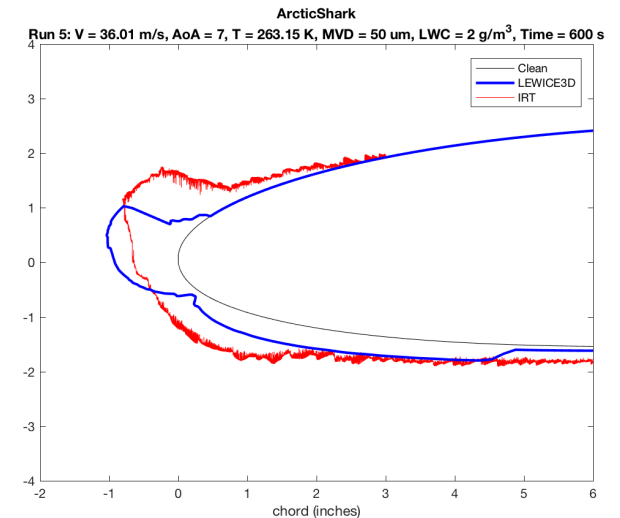
LEWICE3D Data



MVD = 15 μm , LWC = 1.5 g/m³



MVD = 25 μm , LWC = 1.5 g/m³

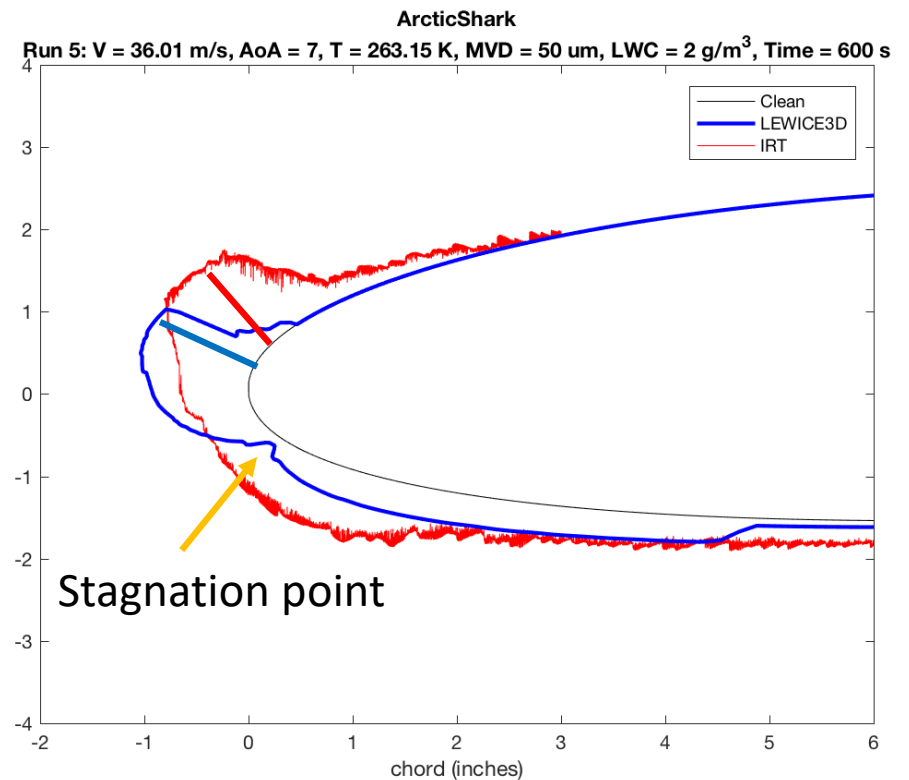


MVD = 50 μm , LWC = 2.0 g/m³



A Closer Look: Glaze Ice

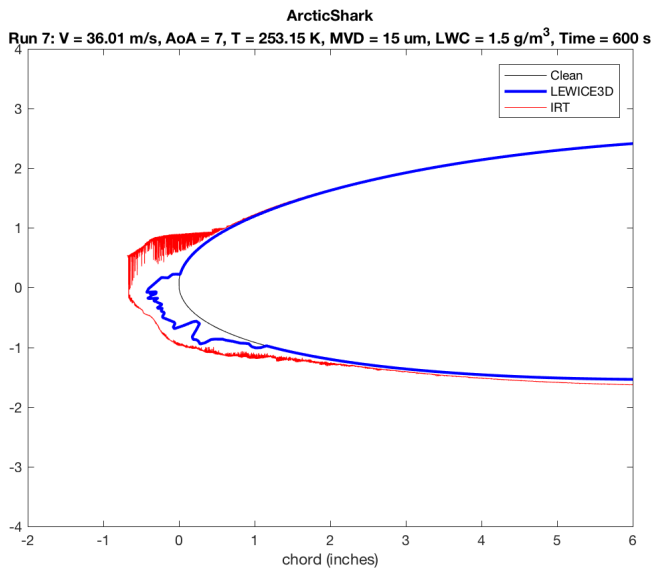
- LEWICE3D has less ice volume (expected b/c IRT data is MCCS)
- LEWICE3D has lower horn angle
- Horn lengths are similar
- LEWICE3D has minimized icing on stagnation point



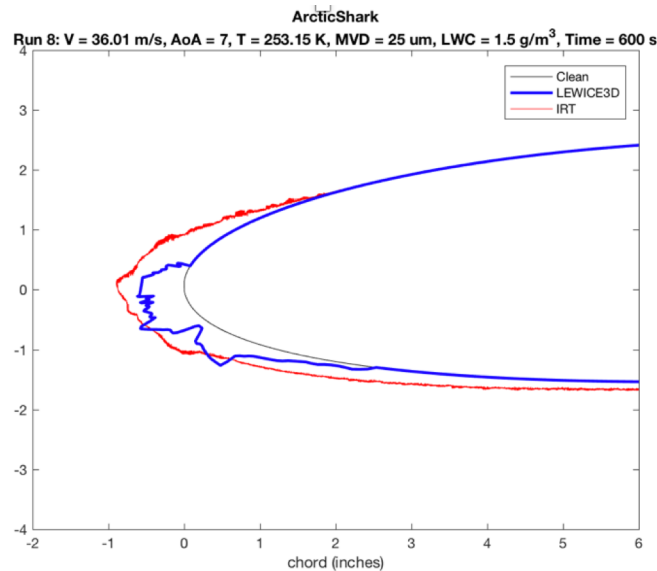


ArcticShark: Rime Ice (-20 C), AoA = 7, V = 70 kts

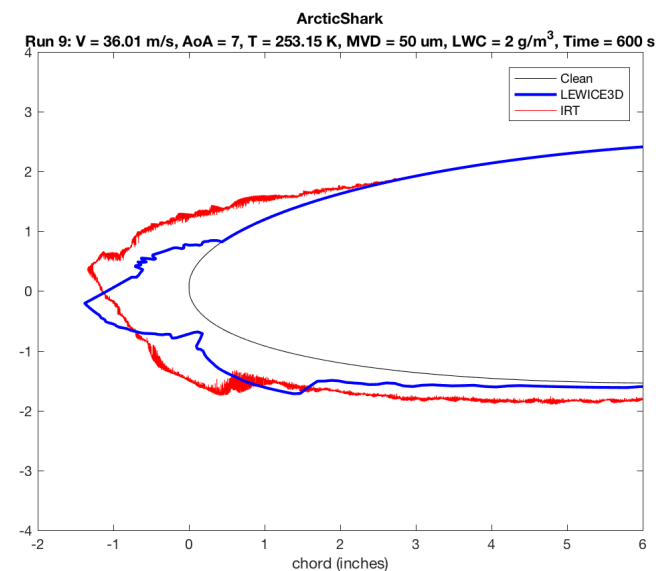
Rime Ice = Water droplets freeze immediately upon impact



MVD = 15 μm , LWC = 1.5 g/m³



MVD = 25 μm , LWC = 1.5 g/m³

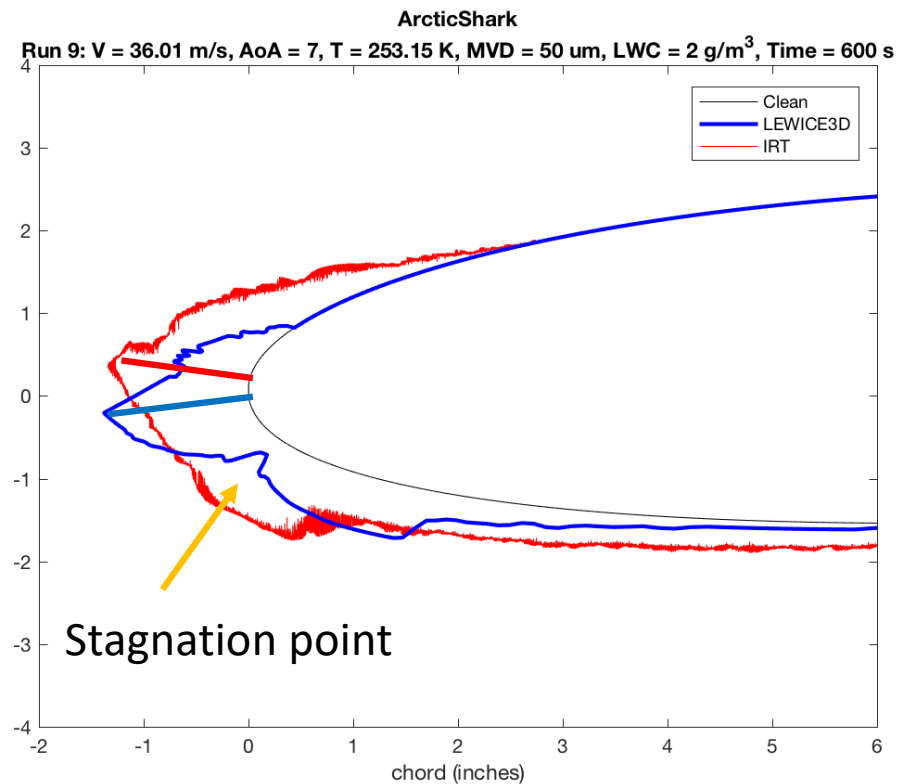


MVD = 50 μm , LWC = 2.0 g/m³



A Closer Look: Rime Ice

- LEWICE3D has less ice volume (expected b/c IRT data is MCCS)
- LEWICE3D has lower horn angle
- Horn lengths are similar
- LEWICE3D has minimized icing on stagnation point





Sources of Errors/Inconsistencies

- Assumed atmospheric pressure in LEWICE3D sims, IRT static pressures vary
- Have not done mesh convergence studies with icing simulations
- Assumed universal droplet size in LEWICE3D, IRT has a drop-size distribution
- IRT is not typically calibrated to low speeds
- LEWICE3D does not use a multi-time-step approach with updated flow fields
- Max Combined Cross Section is not exactly representative of full 3D ice shape
- Flow Angularity and Wall Effects in the IRT
- Surface roughness on test article



Future Research

- Further data post-processing (average cross section, compute volume, etc)
- GLENNICE Full 3D Ice Accretion Software Release in Late 2019
- Another Icing Tunnel Test in November 2018
- Multi-rotor aircraft
- Engine-on testing
- Aerodynamic testing of ice shapes in wind tunnel
- Wind tunnel testing of de-icing strategies (thermal de-icing, icephobic materials, mechanical de-icing)
- Ice sensors coupled with de-icing control systems
- Actual Flight Testing in Icing Conditions



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References

1. Fujiwara, G. and M. Bragg. 2017. 3D computational icing method for aircraft conceptual design. In: 9th AIAA Atmospheric and Space Environments Conference.
2. Potapczuk, M. and A. Broeren. 2017. An Integrated Approach to Swept Wing Icing Simulation. In: 7th European Conference for Aeronautics and Space Sciences.
3. Tim Baker, "*Mesh generation: Art or Science?*", Progress in Aerospace Sciences 2005



Backup Slides



CFD Aerodynamic Flow Field

- Used NASA FUN3D Unstructured Flow Solver
- LEWICE3D uses flow field to solve ice growth calculation in one time-step
- Ideally, use multiple time-steps, updating the mesh and flow field every time
- LEWICE2D does this with 2D inviscid panel method
- 3D Mesh Adaptation and RANS (Viscous) 3D Flow Solution too computationally expensive
- This feature will be implemented in next-generation LEWICE3D (GLENNICE3D)

for every timestep
calculate trajectories using flow field
calculate ice shapes
update mesh based on ice shapes
calculate flow field on new mesh
repeat



CFD WorkFlow

